

FACTORY PREPARED TECHNICAL SERVICE DATA STEREO HI-FI BULLETIN: R49-3

MODEL: CR280

SERVICE PUBLICATIONS DEPARTMENT

Entertainment Products Group - Sylvania Electric Products Inc. - 700 Ellicott Street - Batavia, N.Y.



CHASSIS IDENTIFICATION -----

Chassis Identification consists of two blocks of numbers. In all correspondence relating to a specific model, both blocks of numbers, plus the cabinet model number should be given. To associate a chassis with its proper schematic, refer to the number breakdown described below:

---- CODE CHANGES -----

To assist in identifying changes in electrical components, a system of adding a suffix number to the schematic parts coding number is used. All parts changes are indicated on either partial or complete schematics, and also in the parts list. For example, a part coded "R100" on the initial production chassis changes to "R100-1" when first revised in value; "R100-2" on the second revision, and so on.

- CHASSIS REMOVAL -----

- 1. Remove two (2) screws from bottom of cabinet near sides.
- 2. Remove six (6) screws securing back cover to cabinet.
- 3. Remove four (4) slide control knobs by pulling straight away from escutcheon.
- Control escutcheon is secured to cabinet by spring clips. Remove by pulling away from cabinet at slide control end.
- Remove four (4) screws at outer corners of chassis securing chassis to cabinet.
- 6. Remove chassis and back cover as one unit from front of cabinet.

- LAMP REPLACEMENT ----

Remove chassis. Use #259 bulb, Sylvania Part #30-26288-1 for dial lamp and tuning meter lamp replacement.

Use #45 bulb, Sylvania Part #30-62495-45 for Multiplex lamp replacement.

IMPORTANT: Always use genuine Sylvania replacement parts and tubes.



BULLETIN: R49-3

Price \$1.50



SERVICING THE STEREO HI-FI AMPLIFIER —

Stereo Hi-Fi Amplifier circuits are much easier to service than many other circuits, inasmuch as there are two identical amplifiers right before you for comparison. Use the function switches and controls to locate the trouble area, then pinpoint the defective component within the area.

As an aid to parts identification, blocks of numbers have been assigned to circuits in this chassis - ie:

- 0-200 Block AM/FM MULTIPLEX tuner.
- 300 Block Left Channel Phono Preamp.
- 100 Block Left Channel Phono Preamp.
- 400 Block Right Channel Phono Preamp.
- 500 Block Items common to both L & R Channels.
- 600 Block Left Channel Preamp and Tone Circuits.
- 700 Block Right Channel Preamp and Tone Circuits.
- 800 Block Left Channel Power Amplifier Circuit.
- 900 Block Right Channel Power Amplifier Circuit.

Tuner pins and wire connections are labeled with a single letter whenever possible.

Left and right channel audio amplifier connections are double lettered, with the first letter indicating the channel, ie: LB (Left) or RB (Right).

Visual inspection of components will often disclose overheated parts. A good magnifying glass will be very helpful when checking the printed circuit panel for cracked foil or poor solder joints. Thermal noise may be generated by resistors or transistors that "look like new" as well as other components. Use a heat lamp and aerosol cooler to isolate these troubles.

Remember that schematic voltages are not absolute - they will vary due to normal production tolerances. The primary AC supply (120V, 60Hz) will influence B plus greatly. Compare voltages for the right and left channels when suspecting trouble in a certain amplifier stage. The use of a modern, high impedance VOM, or preferably, a VTVM is a 'must' for checking transistor voltages. Be very careful with your instrument probes when working on transistor circuits - even a momentary short between Base and Collector can destroy the transistor.

Stage gain may be checked by touching the Collector and then

the Base of a transistor with your finger. You will hear a hum from the Collector, and an appreciably louder hum when you touch the Base. Bear in mind that there is no AC voltage gain in the driver and output stages of this amplifier, and also that an inoperative transistor will often pass some signal, but without gain.

A word about replacing solid state devices in these tuner and amplifier circuits - whenever possible, we give the E.I.A. number PROVIDING that the "off-the-shelf" part will restore operation of the instrument to meet factory specifications. However, Sylvania part numbers only are given whenever the transistors or diodes are specifically "paired", or selected for Beta, P.I.V., low noise, etc., and replacement by any "off-the-shelf" item may, or may not, restore operation to meet factory 'specs'.

When servicing Solid State amplifier and tuner circuits, always observe the following rules:

- 1. BE SURE all test equipment is free from leakage and isolated from the power line.
- 2. Use non-inductive dummy loads of at least 3 ohms total resistance 8 ohm loads are nominal. NEVER use single speakers or combinations of speaker systems of less than 3 ohms total impedance. Momentarily shorted or open outputs will not damage the output stages of this amplifier. However, a continuous shorted output condition can cause serious damage within a relatively short period of time.
- 3. Always unplug the power cord from the 120VAC, 60Hz supply before replacing components.
- 4. Use a low wattage, pencil type iron to ensure minimum heat application. Heat sink each lead on solid state devices. An alligator clip will serve quite well as a heat sink in most cases.
- 5. Be sure that mounting surfaces for power transistors are clean and free from burrs. Use silicon grease liberally (both sides of mica insulators when used) when mounting power transistors. Be sure that power transistors are positioned so that the mounting surface is in full, snug contact with the heat sink and that leads clear adjacent chassis or heat sink metal.

---- AMPLIFIER BLOCK DIAGRAM ------



POWER SUPPLY

T502 (power transformer) provides necessary line isolation for this chassis, and also furnishes stepped-down voltages for the bridge rectifier circuit, plus 6.3 volts for dial, meter and stereo lamp operation. All DC working voltages for the amplifier and tuner circuits are supplied by the bridge circuit.

RIPPLE REDUCER

Q502 is used in a "ripple reducer" circuit which removes the B⁺ ripple caused by load current. With a Zener diode (SC500) establishing a 15.6 volt reference for Q502, the circuit output is a clean, constant 15VDC supply for the magnetic preamplifiers (IC502A), the voltage amplifiers (IC502B) and the AM-FM-MULTIPLEX tuner circuits.

INTEGRATED CIRCUIT

This R49 amplifier features a monolithic integrated circuit which contains four operational amplifiers. Each section conof a Darlington input circuit, a differential amplifier, three output transistors, diodes for voltage stability and temperature compensation, plus several resistors.

Two sections of this integrated circuit are used in Left and Right channel magnetic preamp. circuits preceding the function switch. The balance of IC502 serves as Left and Right channel voltage amplifier following the function switch.

It is strongly recommended that the integrated circuit be removed from its' socket before checking associate components for 'shorts', 'opens' or value changes to prevent possible damage to internal IC components.

CONTROLS

R616 (BASS) and R622 (TREBLE) are dual ganged slide-type controls of the conventional passive type used in a normal cutboost tone circuit. These controls permit adjustment of Bass or Treble response of left and right channels simultaneously, while passing the mid-range frequencies (around 1kHz) almost unchanged. Tone control center position gives "as recorded, or transmitted" reproduction.

R610 (BALANCE) control is also of the slide type. It shunts a selected portion of the audio signal to ground, thus equalizing left and right channel outputs.

Design of the dual ganged LOUDNESS slide-type control (R624) with tap compensation is in accordance with the Fletcher-Munson studies, which indicate a definite hearing deficiency at lower frequencies in all average persons, especially at lower listening levels.

POWER AMPLIFIER SECTION:

From the loudness control, the audio signal enters the Power Amplifier panel, and is AC coupled to the Base of a Voltage Amplifier (Q802, Q902). AC and DC feedback from the output stage is applied to the emitter of this voltage amplifier through R806 or R906 to ensure good frequency response with minimal distortion.

BIAS REGULATOR:

The purpose of Q806 is to provide proper bias for the complementary drivers (Q808, Q810) and power output transistors (Q812, Q814), as well as ensuring thermal circuit stability under varying operating conditions. Basically, Q806, R812, R814 and R816 function as a variable diode. Proper bias adjustment consists of adjusting R814 for a reading of 10 to 20 mV across R828 with the loudness control at MINIMUM (to ensure a "no-signal" condition).

When troubleshooting this circuit, NEVER power the circuit without the bias regulator (Q806, Q906) in the circuit. Without the limiting diode action of the bias transistor, the resistor dividing network will supply a voltage of sufficient amplitude to ensure instant destruction of driver (Q808, Q810) and output (Q812, Q814) transistors.

----- CIRCUIT DESCRIPTION (AMP CONT'D) -----

PRE-DRIVER, DRIVER AND OUTPUT STAGES:

Q804 (pre-driver) drives Q808 and Q810 simultaneously. An audio signal of one polarity increases collector voltage of Q804, which in turn increases conduction of the Q808 driver and Q814 output combination. During this half-cycle, Q810 driver and Q812 output combination remain at an idle. The opposite half-cycle reduces collector voltage of Q804, increases conduction of Q810 and Q812 while Q808 and Q814 remain at an idle.

With both driver and output stages biased in class AB, the correct idle current is most important for proper amplifier performance. Insufficient idle current will cause crossover distortion. High idle current will cause low amplifier output.

C806 is a bootstrap capacitor for the pre-driver (Q804) collector. It reduces hum and distortion within the circuit, and also allows the output signal to swing closer to the supply voltage, thus providing slightly higher output.

----- PERFORMANCE ANALYSIS ------

Maintain line at 120V, 60Hz for all tests.

8 ohm, 50 watt resistive load to be connected across each channel output before any of the following performance checks are made.

Adjust bias pots (R814, R914) for $15mV\pm10\%$ across R828, R928 with loudness control set at minimum to ensure "no signal" condition.

SENSITIVITY - PHONO:

CHASSIS equivalent impedance is 330K, 10% resistor with 330 ohm divider.

Adjust controls as follows: Loudness - Maximum. Bass & Treble - Mechanical Center. Balance - Mechanical Center. Select "PHONO" and "STEREO" functions.

Connect a 600 ohm impedance audio generator to both PHONO inputs through correct equivalent impedance.

This chassis requires 6mV $\pm 3db$ at 1kHz for an output level of 1 watt (2.8V - R.M.S. - measures across 8 ohm load resistor). Channel output difference shall be 4 db or less.

SENSTIVITY - TAPE:

Connect a 600 ohm impedance audio generator to both TAPE inputs through 10K, 10% resistors. Adjust controls as under Phono sensitivity. Select "TAPE" and "STEREO" functions.

select "TAPE" and "STEREO" functions.

This chassis required $55mV \pm 3db$ at 1kHz for an output level of 1 watt (2.8V - R.M.S. - measured across 8 ohm load resistor).

TONE CONTROL RANGE:

Connect a 600 ohm impedance audio generator to both PHONO inputs through correct equivalent impedance (See SENSITIVITY - PHONO). Adjust controls as follows: Loudness - Maximum. Balance - Mechanical Center. Bass & Treble - Mechanical Center, initially.

Select "PHONO" and "STEREO" functions.

CONTROL, GEN. FREQ.	CUT	BOOST	
Bass - 100Hz	-9db, ±3db	+10db, ±3db	
Treble - 10kHz	-13db, \pm 3db	+9db, ±3db	

POWER OUTPUT:

Connect a 600 ohm impedance audio generator to both PHONO inputs through correct equivalent impedance (See SENSITIVITY - PHONO).

Adjust controls as follows:

Loudness - Maximum.

Bass & Treble - Mechanical Center, Balance - Adjust for equal R & L channel output, Select "PHONO" and "STEREO" functions.

Adjust generator for amplifier output of 8 watts (8 volts - R.M.S. - measured across 8 ohm load resistor) at each frequency specified.

100Hz - 2% Total Harmonic Distortion (Nominal). 1000Hz - 2% Total Harmonic Distortion (Nominal). 10kHz - 2% Total Harmonic Distortion (Nominal).

CHANNEL SEPARATION:

Apply signal to one phono input, with opposite phono input terminated with appropriate impedance (See SENSITIVITY -PHONO). Adjust controls as follows: Loudness - Maximum. Bass & Treble - Mechanical Center. Balance - Mechanical Center. Select "PHONO" and "STEREO" functions.

Adjust signal generator for amplifier output of 3 watts (5V - R.M.S. - measured across 8 ohm load resistor) on driven channel at each frequency noted below. Measure crosstalk from right into left amplifier, then from left into right.

CROSSTALK LIMITS
40db - typical
30db - typical
20db - typical

HUM AND NOISE: Terminate both phono inputs with appropriate impedances (See SENSITIVITY - PHONO). Adjust controls as follows: Bass & Treble - Mechanical Center. Balance - Mechanical Center. Select "PHONO" and "STEREO" functions.

Measure hum and noise across 8 ohm load resistors.

Loudness control MINIMUM - 1.5mV - Typical. Loudness control MAXIMUM - 25mV - Typical.

Terminate both TAPE inputs with 10K, 10% resistors - select "TAPE" and "STEREO" functions.

Balance, Bass and Treble controls at mechanical center.

Loudness control MAXIMUM - 25mV typical across 8 ohm loads.



CONTROL PANEL (TOP VIEW)



CONTROL PANEL (BOTTOM VIEW)



FUNCTION SWITCH (TOP VIEW)



FUNCTION SWITCH (BOTTOM VIEW)



CAPACITORS



R454 R304 R302 R128 R121 R358 R402 R406 R356 R354 R404 R352 R124 R118 R116 R114R122 R112 R126

RESISTORS



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- MAIN PANEL ASSEMBLY ----



* SEE SCHEMATIC



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- SCHEMATIC DIAGRAM (TUNER) -



SCHEMATIC CODING	SERVICE PART NO.	DESCRIPTION	SCHEMATIC CODING	SERVICE PART NO.	DESCRIPTION
CAPACITORS (All in MFD, unless otherwise specified)		unless otherwise specified)	CAPACITORS (CONT'D)		
C2	42-32806-2	Main Tuning Gang	C136		2200 PF
C8	42-02000-2	330PF	C138		2200PF
C12		330PF	C140		2200PF
		01	C140		2200PF
C14		.01	C142		01
C16		.01	C140		.01
C18		.01	C150	41 22477 05	
C20		.01	C302	41-324/7-85	1/50V Electrolytic
C22		330PF	C304	41-324/7-37	100/15V Electrolytic (Early Prod.)
C24		5.6PF	C 304	41-324//-48	25/25V Electrolytic
C26		12PF, N330	C306		.04/
C28	42-18146-1	1-6PF Ceramic Trimmer	C308		.15
C30		6.8PF	C310	41 -32477 -85	1/50V Electrolytic
C32		330PF	C352	41 -32477 -85	1/50V Electrolytic
C34		.05	C354	41 -32477 -38	250/16V Electrolytic (Early Prod.)
C36		.005	C354	41-32477-48	25/25V Electrolytic
C38		.05	C356	41-32477-46	5/25V Electrolytic
C39		.05	C358		.047
C 42		33PF	C402	41-32477-46	1/50V Electrolytic
C42		001	C 404	41-32477-37	100/15V Electrolytic (Early Prod.)
C44		01	C404	41-32477-48	25/25V Electrolytic
C40		05	C 404	41-52477-40	047
C48		.05	C406		15
C50		2200PF	C408	1. 00 177 05	
C52		.22	C410	41-324/7-85	1/50V Electrolytic
C54	41-23765-5	5/25V Electrolytic	C452	41-32477-85	1/50V Electrolytic
C56		.05	C454	41-32477-38	250/16V Electrolytic (Early Prod.)
C 58		.33PF	C454	41-32477-48	25/25V Electrolytic
C62		.001	C456	41-32477-46	5/25V Electrolytic
C64		.05	C458		.047
C66		.05	C502	43-98665-6	.005/150VAC
C68		.05	C504	43-98665-5	.005/150VAC
C70		10PF	C506		.01
C72		.005	C 508		.01
C74		0056	C510	41-32934-1	1500 x 500 x 200 Electrolytic
C76		05	C513		.22
C78		01	C514		.22
C70		05	C 525	13-97665-6	005/150VAC
600		220PE	C610	43-77003-0	0027
C02		220 PE	C612		047
084		22077	C612		200PE
686		330PF	C014		2000 BE
C88		330PF	C010		000
C90	41-23765-5	5/25V Electrolytic	C618		.022
C92		.01	C/10		.002/
C94		.05	C712		.047
C96		.05	C714		820PF
C100		.05	C716		3900PF
C102		.01	C718		.022
C104		.01	C802		.047
C105	41-29270-5	5/25V Electrolytic	C803		220 P F
C1 06		.05	C804	41-23765-7	25/25V Electrolytic
C107		220PF	C806	41-23765-7	25/25V Electrolytic
C1 08		100PF	C807		220PF
C110		001	C808		47 PF
CIII		05	C809		220PF
CIII	41 22765 16	1/50V Electrolutio	C810	41-32477-67	500/35V Electrolytic
C112	41-23/03-10		C010	41-524/7-07	047
C113		1500 DE	C902		220 PE
CIIS		1500FF	C903	11 007/5 7	
C116			C 904	41-23/03-/	
	41-23/65-16	1/50V Electrolytic	C 900	41-23/03-/	
C118		2700PF	C907		220PF
C120	40-10285-8	10,000PF, 5% - 125V	C 908		4/ FF
C122	40-28121-1	10,000PF, 5% - 125V	C909		220PF
C124		1500PF	C910	41-32477-67	500/35V Electrolytic
C126		.22		1210 22 20 120 120 120 1	
C127		.22	RESISTORS	(All Carbon, 1/	2W, 10% unless otherwise
C128	40-10285-32	1300PF, 5% - 125V		specified)	
C129		.01		era una productiva en estador de California (* 10) Una	
C1 30		2700 PF	R4		680
C130	41 20270 5	5/25V Electrolutio	R6		150
C131	41-272/0-3		R10		100 1 /4Watt
C132	(0.10005.10		D11		4.9K
C134	40-10285-13	3300FF, 5% - 125V (use			0.0K
		w/50-205/9-2 Xtmr.)			2./ N
C134	40-10285-40	5600PF, 5% - 125V (use	K14		
		w/50-32591-1 Xfmr.)	K10		2./K

- REPLACEMENT PARTS LIST (CONT'D)

SCHEMATIC CODING	SERVICE PART NO.	DESCRIPTION	SCHEMATIC CODING	SERVICE PART NO.	DESCRIPTION
RESISTORS	5		RESISTORS	S (CONT'D)	
R18		10K	R 302		100K
R20		3.9K	R304		47
R22		100K, 1/4Watt	R 306		1.8K
R24		l meg.	R352		270K
R 26		68K	R354		47 K
R28		1 K	R 356		68
R30		6.8K, 10%	R358		3.3K
R31		270	R360		10K
R32		1.2K, 5%	R402		100K
R34		120	R404		47
R 36		470	R406		1.8K
R 38			R452		270K
R40			R454		4/K
R42		2.2K	R 4 56		08
R 44		470 22K 59	R458		3.3N
R 40	27 14574 11	120K Thumhurhead ACC Mater Adi	R460		2.2 200
R 40	37-14370-11	470	R 502		3.3 meg, 20%
R 50		120	R 505		8 2K
R52 R53		2.2K	R508	36-62455-57	220 10 Watt
R54		3 9K 5%	R510	30-02433-37	22.0, 10 wall
R56		10K	R512		180
R 58		270	R516		16
R60		1.8K	R518		1.5K
R62		560	R530		18K (Early Prod.)
R64		560	R530		27K
R66		1K, 1/4Watt	R536		47 K
R68		470	R538		47 K
R70		120, 1/4Watt	R540		47K
R72		560	R 542		47 K
R74		560	R544		220
R76		6.8K, 5%	R 546		220
R78		6.8K, 5%	R 548		82
R82		١ĸ	R610	37-32453-1	500K Balance Control
R84		1.8K, 5%	R614		33K
R86		100, 5%	R616	37-32452-2	250K Dual Bass Control
R88		1K	R618		10K
R92		15K	R620		22K
R94		8.2K	R622	37-32452-2	250K Dual Treble Control
R96		5.6K	R624	3/-32452-1	500K Dual Loudness Control
R 97		880	R020		131
R 70		491/	R/14 D719		33K
R 99		100K	R710 P720		224
R101		180K	R720		15K
R102		22K 5%	R802		560K 1/4 Watt - 5%
R104		180K. 5%	R804		680K, 1/4 - 5%
R106		560K	R806		22K, 1/4 Watt
R108		470K	R808		6.8K
R110		39K	R810		100, 5%
R112		180K, 5%	R812		820
R114		68K, 5%	R814	37 -1 4576 -5	1K Thumbwheel Pot - Bias Adjust
R116		330, 5%	R816		560
R117		180K	R818		4.7K
R118		1.8K	R820		4.7K
R120		1.8K	R822		120
R121		22K	R824		120
R122		TUK	R826	04 404541	
R123		6.8K	R828	36-62454-1	I ohm, 5 Watt
R124		270K	R902		500K, 1/4 Watt - 5%
R125		2.24	R 904		20K 1/4 Watt - 5%
D120		1.5K	D 0 00		22N, 1/4 Wall
R130		2.2 abms 5%	R910		100 5%
R132		10K	R912		820
R134		10K	R914	37-14576-5	1K Thumbwheel Pot - Rice Adjust
R136		10K	R916	0/ 140/0-0	560
R138		10K	R918		4.7K
R140		82K	R920		4.7K
R142		82K	R922		120
R144		18K	R924		120
R146		18K	R926		100
R148		15K	R928	36-62454-1	1 ohm, 5 Watt

- REPLACEMENT PARTS LIST (CONT'D) -----

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SCHEMATIC	SERVICE		SCHEMATIC	SERVICE	
CODING	PART NO.	DESCRIPTION	CODING	PART NO.	DESCRIPTION
SOLID STA	TE DEVICES		COILS & T	RANSFORMERS	(CONT'D)
IC 502	1.5-34005-1	Dual Channel IC - Early Prod.	L17	22-28072-2	Ferrite Bead
10502	15-34202-1	Dual Channel IC	L18	50-18789-3	5.7mH Choke
116	22-28072-2	Ferrite Bead	119	22-28072-2	Ferrite Bend
117	22,28072-2	Ferrite Bead	1.20	50-15318-1	2711H Chake
	22-20072-2	Ferrite Bead	1.22	27-22258-1	Loop Loop Core AM (Early Bood)
L17	22-200/2-2	Ferrite Beed	1 22	17 20250 0	Loop - Iron Core AM (Early Froa.)
	22-200/2-2	Franke Dead		2/-32330-3	- Iron Core AM
L30	22-200/2-2			50-20413-1	LOIT - AM RF
	13-20034-1	гмкг Атр.		50-3230/-1	- SCA Trap
Q4	13-32300-1	FM Mixer	L30	22-280/2-2	Ferrite Bead
Q6	3-32364-1	FM Uscillator	L502	50-26001-3	1000H Choke
Q8	13-32366-2	Ist AM/1st FM IF	12	50-26573-1	FM Balun
Q10	13-32366-1	2nd AM/2nd FM IF	T4	50-26580-8	Transformer - 1st FM IF
Q12	13-32366-1	3rd FM IF	Т6	50-26580-9	- 2nd FM IF
Q14	13-32366-1	4th FM IF	T8	50-26580-10	- 3rd FM IF
Q16	13-29033-3	Voltage Amp	T10	50-26584-1	- Ratio Detector
Q18	13-29033-3	Muting Amp	T12	50-26583-3	- 1st AM IF
Q 20	13-32362-1	AM RF Amp.	T14	50-26583-4	- 2nd AM IF
Q22	1.3-18951 -1	AM Converter	T16	50-28411-1	- AM Oscillator
Q24	13-18365-1	Composite Amp	T18	50-26575-1	- 19kHz
Q 26	13-18365-1	38kHz Amp	T 20	50-26579-2	- 38kHz (use w/3300PE
Q 502	13-28471-1	Ripple Reducer			
Q802	13-26386-3	Voltage Amplifier	T20	50-32501-1	- 39kH- /use w/5400PE
Q804	13-34001-1	NPN Darlington	120	50-52571-1	- 30KH2 (Use w/ 5000FF
Q806	13-29033-3	Bias Regulator	T 500	55 20070 1	Cap.)
Q808	13-34003-1	Driver	1 302	33-32972-1	- Power
0810	13-34004-1	Driver			
0812	13-34002-1	Power Output	MISCELLA	NEOUS PARIS	
0814	13-34002-1	Power Output			
0902	13-26386-3	Voltage Amp	CB502	29-33346-8	Circuit Breaker (1.25A)
Q 70Z	12 24001 1	MPN Devilation	SK504	73-15073-1	Socket - Aux, Power
0904	13-34001-1	Rice Resulter	SK506,SK508	73-98079-2	Dual Phono Socket - PHONO IN
0,906	13-29033-3	Dias Regulator	SK510,SK512	73-98079-2	- REM. SPKRS.
Q908	13-34003-1	Driver	SK514,SK516	73-98079-2	- TAPE IN
Q910	13-34004-1	Driver	SK518,SK520	73-98079-2	- TAPE OUT
Q912	13-34002-1	Power Output	SK522,SK524	73-98079-2	- MAIN SPKRS.
Q914	13-34002-1	Power Output	SK 526	73-26338-3	Headphone Jack
SC2	1N3182	Diode - Varicap	SW 502	33-28756-1	Complete Function Switch Asm.
SC4	1N295	- Meter Protection		33-28756-105	AFC Switch Section Only
5C6	1N295	- AM Detector		33-28756-104	AM or FM SwitchSection Only
SC8,SC10	1N542MP	- Ratio Det. (MATCHED PAIR)		33-28756-100	ON-OFF/AUTO Switch Section Only
SC12	13-27596-5	- Rectifier		33-28756-102	PHONO or TAPE Switch Section
SC14	1N295	- 19kHz Doubler		•• •••	Only
SC16	1N295	- 19kHz Doubler		33-28756-101	STEPEO Switch Section Only
SC18	13-17596-5	- Clamp	58504	89_14500_1	Lever Switch Arm - Speaker Select
SC20	13-17596-5	- Muting Switch	SWEND	22 044 29 1	MITE CI:Ja Suita-L
SC22	13-17596-5	- Multiplex Matrix	54 500	72 24021 2	Antones Terminale SM
SC24	13-17596-5	- Multiplex Matrix		73-20731-2	
SC26	13-17596-5	- Multiplex Matrix		73-33071-41	Cord - AC Power
5028	13-17596-5	- Multiplex Matrix		70-99257-4	Dial - Clip (tape-to-carriage)
50302	13-17596-5	- Overland Protect-		//-34029-1	- Drive Spring
SC 402	13-17596-5	- Overland Protect		86-28943-1	- Light Box
50500	13-14979-5	- Zeper		74-28921-2	- Light Diffuser
50500	12 20145 1	- Pectifier		74-28922-5	- Tope (Tuning Indicator)
50502	13-27103-1			77-28439-1	- Tape Drive Spring
30304	13-27103-1			86-28436-2	- Tape Holder
50506	13-29103-1	- Rectifier		86-28433-1	- Tape Roller
SC 508	13-29165-1	- Rectifier		86-28434-1	- Tape Roller Holder
SC802	13-17596-7	- Bias		85-28937-9	Jack Plate
SC 902	13-17596-7	- Bias		30-26288-1	Lamp - Dial & Meter (#259)
SCR2	13-18924-1	- \$.C.R.		30-62495-45	- Multiplex Ind. (#45)
	72-27200-3	Large 3 pin Transistor Socket		73-28247-7	Socket - Dial Lamp
	86-28669-1	Power Xistor - Mica Insulator		73-32463-1	- Meter Lamp
	72-28852-1	- Socket		73-26694-1	- Multiplex Lamp
	70-28659-1	- Mounting Clip		70-84346-25	- Mounting Ring (mpx, & meter
	72-27200-1	Small 3 pin Transistor Socket			lamp)
		_		25-22604-4	Tuning Meter - Early Prod.
COILS AND	TRANSFORME	RS		25-22604-7	+ Later Prod.
				70-26679-1	- Mounting Nut
L2	50-26574-14	Coil - FM RF		74-28923-1	Tuning Thumhwheel - w Ateral State
L4	50-10260-4	- 2.2UH		70-14098-1	Nulas Dastron
1.8	50-11378-5	- 3.3UH		/	- Nyion bearing
	50-26574-15	- EM Interstone			
114	50-26574-19	- FM Oscillator			
115	50-18789-3	- 5 7mH Chake			
	30-10/07-3 33 30073 3	- J./ mill Choke			
LIO	22-200/2-2	nerrite Dega			



CIRCUIT DESCRIPTION (TUNER) -

This tuner shares a printed circuit panel with the amplifier circuits. The R49 tuner covers both the AM broadcast band (540 -1610kHz) and FM broadcast band (87.9 - 108.5MHz).

Especially noteworthy from a servicing standpoint are the top and bottom roadmaps on the printed circuit panel and the use of socket mounted transistors throughout.

The tuner supply voltage (plus 15V) is taken from the amplifier supply and applied to the tuner through a ripple reducer circuit (Q502) and regulated by SC506, a Zener diode.

Q8, Q10, Q16, Q18, Q20, Q24 and Q26 receive power (plus 15V) whenever the amplifier is switched on. Q2, Q4, Q6, Q12 and Q14 receive power only when the FM function is selected; Q22 receives power only when the AM function is selected.

As the FM pushbutton is depressed, the rear D.P.D.T. portion of the switch applies power to selected circuits as outlined above. Simultaneously, the front D.P.D.T. portion of the FM switch removes ground from pin L (FM MONO output). FM audio travels through the STEREO/MONO switch (rear section) through the FM switch (front section), through the TAPE switch (front section), to pins LE (left channel input) and RE (right channel input). The Stereo FM outputs (pins P and Q) remain floating.

Stereo FM reception is very similar, except that pins P and Q are connected to the circuit through the rear section of the STEREO/MONO switch when the switch is depressed, and pin L remains floating.

FM PERFORMANCE

Useable FM Sensitivity (I.H.F.) @ 106MHz	2.5uV
20db Quieting (106MHz)	1.6uV
Image Rejection @ 106MHz	60db
Distortion at 75kHz deviation (400Hz) 1100uV Input	0.6%
Maximum FM S/N ratio (75kHz dev., 1100uV Input)	60db
Stereo Separation (1kHz)	28db
Maximum Output (100% modulation @ 400Hz	.47V-RMS

Maximum Output (100% modulation @ 400Hz

FM RF, OSCILLATOR and MIXER STAGES

RF Signals pass through the FM balun (T2) to the first tuned circuit formed by L2 and the first section of the main tuning gang. The tank circuit is a frequency selective circuit which allows only a small band of frequencies to pass. The selected frequencies are then applied to the gate of Q2, a N channel field effect transistor, for amplification. The output of Q2 passes through a second tuned circuit (C2C, L10) which gives even more frequency selectivity. The signal is then AC coupled to the base of Q4 - the FM Mixer stage. A locally generated unmodulated signal is produced in the FM oscillator circuit of Q6. The oscillator frequency is determined by the tank circuit formed by L14 and the third section of the tuning gang C2E. The oscillator signal is AC coupled to the emitter of Q4. Mixing or heterodyning of the RF and oscillator frequencies in Q4 produce the 10.7 mc IF frequency. Correction of minor frequency drift is the function of the varicap diode. A variation in the detected signal, which contains a DC component as well as audio frequencies, changes the bias on SC2, and thus effectively changes the capacity across L14.

FM IF and DETECTION

There are four FM IF stages in the R19 chassis, two of which share transistors with the AM portion of the receiver. T4, T6 and T8 are tuned to 10.7MHz - the IF frequency. Note the Beads, L16, L17, L19 and L21 shown on the Base leads of the IF amplifiers. Although drawn as a R/L circuit, they are small Ferrite Beads which are slipped over the transistor Base leads before the transistors are inserted in their sockets. At normal IF frequencies, these 'beads' have no effect on the circuit. However, they effectively trap out high frequency parasitic oscillations.

The output of the last IF is applied to the primary of the Ratio Detector (T10). With a frequency modulated signal, audio frequencies will develop in the tertiary winding of T10, and will appear at pin Z.

MONO FM OUTPUT

Composite audio takes two separate paths upon leaving the ratio detector (pin Z). The primary path is through R110, C110 and to the Base of the composite amplifier (Q24). The composite signal is amplified by Q24, passes through the primary of T18 and then through the SCA trap. Note that this trap (L28)

— CIRCUIT DESCRIPTION (TUNER CONT'D) —

is tuned at 72kHz for optimum performance. The audio, now with SCA information removed, travels to the tuner output (pin L) through a deemphasis network.

Some of the detected signal is shunted through the AFC switch section (SW502) to a low pass filter formed by R108 and C34. The detected signal contains audio frequencies as well as a DC component and the low pass filter (C34, R108) filters out all audio from the detected signal. The remaining DC component is used to vary the bias on SC2 - see FM RF, OSCILLA-TOR and MIXER. There should be no audio present at SC2.

AUTOMATIC STEREO SWITCHING

As a transmitted FM signal grows weaker, the background noise level increases. When the noise level reaches 100mV at pin Z, stereo FM reproduction becomes objectionably noisy due to circuit requirements, although Mono FM reproduction is still clear. Therefore, the composite signal is also AC coupled to the Base of Q16. With at least 100mV of noise at pin Z, the noise portion of the composite audio is amplified by Q16, rectified by SC12 and applied to the Base of Q26. The output of Q16 varies the Base voltage of Q26 from -9V (no signal, all noise) to plus 3.4V (good, solid signal). Therefore, under weak signal conditions, Q26 is biased off and there is no 38kHz signal to switch the multiplex diodes off. The FM MONO signal applied at the center tap of T20 passes through the multiplex matrix and appears at output pins P and Q (FM Stereo Outputs).

A marginal Stereo FM signal level could cause this receiver to switch back and forth between Mono and Stereo. SC18 rectifies the 38kHz signal at the collector of Q26 and increases the 15 volts at C129 to approximately 30 volts. This increased voltage further biases Q26 on, which in turn would require a higher output from Q16 to turn Q26 off again. SC18, therefore, ensures that automatic MONO/STEREO switching will not take place with less than a 2.9uV signal.

FM MUTING

The FM muting circuit has no adjustments. The circuit is completely disabled when the FM muting switch is in the "OFF" position. Switching FM muting "ON" will reduce FM off-station noise by 25 to 30db.

With the receievr tuned off-station, there is a large amount of random noise presented to Q16 for amplification. This amplified noise is rectified by SC12, producing a negative 17VDC at the MUTE switch. Closing this switch (SW508) applies this negative DC voltage to the Base of Q18 (Muting Amp). With Q18 biased off, R102 is, in effect, removed from the circuit. This causes the DC voltage on the anode of SC20 to increase. With SC20 reverse biased, the noise must now pass through C113 and R106 - resulting in attenuation of the noise. The Base voltage of Q24 rises, which is reflected by a decrease to 8 volts of the potential at point Y.

Upon tuning to a station with 3uV or greater signal strength, the background noise is reduced, so that Q18 turns on. SC20 now switches on and passes unattenuated audio to the Base of Q24. The Base voltage of Q24 now drops, which is reflected by the point Y voltage rising to 9.9V. This results in Q18 being turned on still harder. Due to the voltage action at point Y, marginal signal levels will not cause the FM muting circuit to switch in and out with minor signal strength variations.

C115 and C117 slow down the muting action to prevent speaker

"pop". Q16 and SC12 are the key components for correct muting action.

STEREO INDICATOR LAMP

A 19kHz signal is present only during a stereo broadcast - See STEREO FM. A portion of the 38kHz signal present at the Collector of Q26 is AC coupled to the Gate of a Silicon Controlled Rectifier, SCR2. The anode of this SCR is connected to 6.3VAC through a #45 Stereo Indicator Lamp.

With approximately 16V(P/P) of 38kHz signal at the collector of Q26, the SCR is switched on, causing the Stereo Indicator Lamp to light.

AGC AND TUNING METER

AM AGC is developed from the IF signal at T14 secondary.

FM AGC is obtained from a "sampling" of the 10.7 IF at the collector of Q10 by C70.

The AM or FM signal is rectified by SC6 and applied to the base of Q8 through T12 and T4 secondary.

AGC adjustment consists of adjusting R48 so that the tuning meter needle rests on the first dot on the low end of the scale with no signal input.

With the AGC correctly set, the negative voltage from SC6 varies in direct proportion with the received signal strength. A strong signal will reduce the voltage on the base of Q8, reducing FM stage gain, and also cause Q8 emitter voltage to drop. The decrease in emitter voltage causes the tuning meter needle to deflect up-scale, and is also applied to the base of Q4 (FM Mixer) for further FM gain control.

With the receiver in the AM mode of operation, the rectified FM signal controls Q8, and the Q8 emitter voltage is applied to the base of Q20 (AM RF Amplifier), resulting in stage gain reduction under strong signal conditions.

AM PERFORMANCE

Sensitivity for 20db S plus N/N @ 1400kHz	110uV/M
Sensitivity for 50mV output @ 1400kHz	80 uV/M
Image Rejection @ 1400kHz	82db

AM OPERATION

RF signals are picked up by the first tuned circuit formed by the Ferrite rod antenna (L23) and the AM RF tuning gang section, C2F. This tank circuit is frequency selective, and allows only a narrow band of frequencies to pass. These selected frequencies are directly coupled to the Base of Q20, the AM RF amplifier. The output of Q20 passes through a second tuned circuit (C2H, L24) which gives even more frequency selectivity. This signal is then AC coupled to the Base of Q22, AM converter.

Q22 also acts as an oscillator, with frequency determined by a tank circuit consisting of T16 and C2K. The selected incoming frequency is mixed with the oscillator frequency to produce the 455kHz "difference" frequency for the first AM IF stage. The selected frequency is amplified by two IF stages, detected by SC6 and coupled through C92 to the audio amplifier.

----- CABINET REPLACEMENT PARTS LIST -----

DESCRIPTION	SERVICE PART NO.	DESCRIPTION	SERVICE PART NO.
Bezel - Control	74-28947-2	- Pushbutton Insert	74-34084-1
- Control Overlay	74-28946-3	- Slide Button	74-28751-1
- Dial	74-28944-1	Cabinet - Back Cover	85-32326-3
- Mounting Clip	70-28855-1	- Foot, Plastic	86-91119-3
- Pushbutton	74-32308-4		

ALIGNMENT PROCEDURE —

GENERAL

This receiver has been factory aligned with precision laboratory equipment. The circuits are quite stable, and not normally subject to drift. Therefore, check all circuits for malfunctions before attempting realignment. Realign ONLY when absolutely necessary.

Maintain line voltage at 120V, 60Hz during alignment.

All R.F. shields must be in place during alignment.

ALWAYS KEEP ALIGNMENT SIGNALS AT THE LOWEST USEABLE LEVEL DURING ALIGNMENT. During FM alignment maintain input signal below tuner limiting level. Note the generator attenuator setting at which further input signal increase does not increase the output. Keep the input signal below this point.

8 ohm, 50 watt non-inductive loads are required for L & R channel amplifier output terminals if speaker systems are disconnected.

Set tuning dial indicator at zero (0) on the logging scale with tuning capacitor (C2) set at maximum capacity. NOTE: Readjusting tuning dial indicator after AM or FM alignment will make RF realignment (AM & FM) necessary for correct station calibration.

Adjust tuning meter needle to first dot on the low end of the scale (no signal input) with thumbwheel pot R48 before beginning alignment.

FM RF and IF sections must be properly aligned before beginning multiplex FM alignment.

EQUIPMENT REQUIRED:

AM:

AM signal generator capable of 400Hz, 30% modulated, accurate signals from 455kHz to 1610kHz.

50 ohm IF probe - see probe #1, pg. 22.

AC VTVM or general purpose scope capable of indicating approximately .05 volt, 400Hz audio.

FM:

FM signal generator capable of 400Hz, 30% (221/kHz deviation) modulated, accurate signals from 87.9MHz to 108.5MHz.

IF sweep generator, capable of sweeping 300kHz, 10.7MHz center frequency.

Accurate markers for 10.6, 10.7 and 10.8MHz.

50 ohm IF probe - see probe #2, pg. 22.

Detector probe - see probe #3, pg. 22.

Matching 300 ohm balun or pad for RF input, unless FM signal generator has balanced 300 ohm output. See pg. 22.

VTVM with low DC scale.

General purpose scope capable of displaying IF response curve of approximately 40mV.

MULTIPLEX FM:

Multiplex generator with the following capabilities: 1.72kHz (SCA) modulated signal. 2. Standard multiplex signal, 400Hz modulation.

Oscilloscope - preferably dual trace.

Matching 300 ohm balun or pad for RF input unless multiplex generator has balanced 300 ohm output. See pg. 22.

STEP	TUNING CAPACITOR SETTING	TEST EQUIPMENT HOOK-UP	GENERATOR FREQUENCY	AD JUSTMENT POINT	ADJUST FOR	
1	At point of no interfer- ence.	Generator to Pin X through probe #1. Scope or VTVM to AM output - Pin K .	455kHz mod- ulated 30% with 400Hz.	T14 T12 T12 Top	Maximum 400Hz Output,	
NOTE: Repeat	T12 resonates until further adj	at two core positions. Tune both cores to ou ustment does not increase output.	ter peaks.			
2	1400kHz	Radiate RF signal from generator. Scope or VTVM to AM output - Pin K.	1400kHz mod- ulated 30% with 400Hz.	C2L	Correct tuning dial reading at 1400kHz.	
3	600kHz		600kHz modu- lated 30% with 400Hz.	[T16]	Correct tuning dial reading at 600kHz.	
Repeat	steps 2 and 3 ur	ntil proper tracking is achieved.				
4	1400kHz	Radiate RF signal from generator. Scope or VTVM to AM output - Pin K.	1400kHz modu- lated 30% with 400Hz.	C2J C2G	Maximum 400Hz Output.	
5	600kHz		600kHz modu- lated 30% with 400Hz.	L24 L22 Link	Maximum 400Hz Output,	
Repeat When co	Repeat steps 4 and 5 until further adjustments do not increase output. When correctly aligned, this receiver will tune through a carrier at 540kHz and 1610kHz.					

- AM ALIGNMENT -----

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----- FM ALIGNMENT -----

			·	·····		
STEP	TUNING CAPACITOR SETTING	TEST EQUIPMENT HOOK-UP	GENERATOR FREQUENCY	AD JUSTMENT POINT	ADJUST FOR	
NOTE:						
1	Point of no interference.	Sweep Generator - to base of Q8 through probe #2. Use 10.6, 10.7 and 10.8MHz markers. Scope - to Pin V through probe #3.	10.7 MHz sweep and markers.	T8BottomT8TopT6BottomT6Top	Maximum gain, proper markers.	
2		Sweep Generator - to base of Q4 through probe #2. Use 10.6, 10.7 and 10.8MHz markers. Scope - same as step #1.		T4 Bottom T4 Top	See Fig. A.	
3		Sweep Generator - same as step #2. Use 10.7 marker only.	1	T10 Bottom	Maximum gain of "S" curve,	
		Scope - to Pin Z - Ratio Detector output,		[<u>T10]</u> Top	Marker centering on "S" curve. See Fig. B.	
DC Volt	tage at Pin Z s	should be Zero with no signal input. Readjust	t top core of T10	SLIGHTLY to obtain zero	, if necessary.	
4	106MHz		106MHz modu- lated 30% (22½kHz dev.) at 400Hz.	C28	Maximum output (400Hz) at 106MHz.	
5	90MH <i>z</i>	Signal Generator - to FM antenna terminals Use 300 ohm pad or balun, if necessary, for balanced input. Scope - to Pin L - Mono FM output.	90MHz modu- lated 30% (22½kHz dev.) at 400Hz.	L14	Maximum output (400Hz) at 90MHz.	
Repeat	steps 4 and 5 ur	atil proper tuning dial tracking is achieved.	۸		1	
6	106MHz	Signal Generator - same as step 4.	Same as step 4.	C2D C2B	Maximum 400Hz Output.	
7	90MHz	Scope - same as step 4.	Same as step 5.	L10 L2	Maximum 400Hz Output,	
Repeat	steps 6 and 7 ur	ntil further adjustment does not increase outp	nit.			
The AF recheck	C should "pull i alignment,	n" a FM station equally well on both sides o	f the center frequ	ency when switched on. If	it does not do so,	
8	8 Off-station. Scope to Pin L - Mono FM Output Operate SW508 - Mute switch, Noise signal will drop 25-30db with muting action.					
When correctly aligned, this receiver will tune through a carrier at 87.9MHz and 108.5MHz.						

- MULTIPLEX ALIGNMENT -----

STEP	TEST EQUIPMENT HOOK-UP	GENERATOR FREQUENCY	ADJUSTMENT POINT	AD JUST FOR			
SCA TRAP A	SCA TRAP ALIGNMENT						
I	Multiplex Generator to Antenna Terminals - Use 300 ohm pad or balun if needed. Scope to Pin Y.	72kHz	L28	MINIMUM RESPONSE			
19kHz PILO'I	ALIGNMENT						
2	Multiplex Generator - same as step #1. Scope to Pin CC .	10% 19kHz Pilot, modulation off.	T18 Bottom T18 Top T20	MAXIMUM 38kHz, see schematic.			
NOTE: T18	NOTE: T18 resonates at two core positions, Tune both cores to OUTER peaks.						
MULTIPLEX SWITCHING							
3	Multiplex Generator - same as step #1. Scope to Pins P and Q . Use input signal level of 200uV.	Full Multiplex signal, one chan- nel modulated.	[T20]	Best cha nnel separation.			

